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# METHOD FOR EXTRACTING AND RECYCLING WASTE CHEMICALLY TREATED WOOD

This invention relates to the extraction, decontamination and defibration of waste chemically treated (contaminated) wood with a one-step process that yields fibres suitable for the production of lignocellulosic composite materials.

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By chemically treated wood is meant exterior-use wood which has been impregnated in the past with chemicals (i.e. preservatives) - some of them being hazardous - such as creosote, salts of chromium, copper and arsenic (CCA), pentachlorophenol (PCP) and others. Such a chemical treatment is carried out in order to protect wood and make it durable against long term deterioration, weathering and natural ageing. In general, chemically treated (contaminated) wood has been used in the applications of construction and garden timber, electricity poles, telecommunication poles, railway sleepers, posts, etc.

Gilbert et al. (U.S. 5.262.004, 1993) developed a 25 method for extracting chemical preservatives from treated wood by chipping, impregnating with alkali, treating with saturated steam, explosive decompression and refining in a crusher permitting the grinding of wood. This technology never reached to the pilot-scale level due to 30 its multiple-step operation and complexity.

Levien et al. (U.S. 5.364.475, 1994) invented a process based on a supercritical fluid extraction for recycling waste treated wood. Such wood is chipped and stripped so that the core can separately be processed since it contains less or no contaminants. The rest of it

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is subjected to a supercritical fluid (SCF) treatment at high and moderate temperatures. Main disadvantage of the process is the use of carbon dioxide and methanol as modifiers, while the equipment required is very 5 expensive.

Fransham et al. (U.S. 5.378.323, 1995) developed a method and apparatus for removing oil- and tar- based wood preservatives from sawdust. The efficiency of the method is questionable, while it requires high energy 10 consumption for shaving and dusting the treated wood.

Korfiatis and Pal (U.S. 5.629.199, 1997) claimed a sonically enhanced method for removing creosote and PCP from treated wood products. In this process, treated wood is disintegrated to produce chips that are then contacted with an organic solvent, preferably methanol, and sonicated to extract the contaminants. The efficiency of the process is limited to an extraction degree of approx. 94-96% which is obtained after long treatment times (10-12 hours).

Ruddick and Cui (U.S. 5.476.975, 1995) developed a method for extracting organic toxic contaminants such as PCP, polychlorinated dibenzo-p-dioxins, etc. from wood with a supercritical fluid such as carbon dioxide and use of an entrainer such as methanol or ethanol. The process requires times of 4-5 hours for a relatively efficient extraction and applies very high pressures.

Portier et al. (Microbial-assisted remediation of creosote- and pentachlorophenol- treated wood products, Journal of Industrial Microbiology, Vol.17, 1996, p. 1-5)

30 reported on a new lab scale recycling method for waste creosote- and pentachlorophenol- treated wood, that consists of an extraction with methanol and a bio-

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polishing with a microbial consortium containing specific adapted strains.

and Boehme (U.S. 5.804.035, Michanickl 1998) developed a process for recycling waste particleboards fibreboards. In this process, which discontinuous process, chipped waste boards are treated with steam and additives such as urea and dilute mineral acids at temperatures around 120°C. The chipped boards disintegrate completely. Thereafter, this 10 material is dried in a conventional dryer and processed usual for the production of particleboards. experience exists on using waste treated wood. process is used today industrially to recycle only waste urea-formaldehyde bonded particleboards.

15 In the present application, it is described a method extracting, decontaminating and defibrating waste chemically treated wood of different types by subjecting it to a chemical-thermal treatment at from 40 to 100°C accompanied by a mechanical treatment with high shear 20 forces which defibrate the wood. The resulting clean and extracted fibres can be formed into composites, example, dry process fibreboard, wet process low density fibreboard (softboard), wet process high density fibreboard (hardboard), special particleboard having such recycled 25 fibres in the core layer, and other moulded products, by bonding, if necessary, with conventional synthetic resins. The extent of the high shear treatment, temperature and composition of chemical reagents required for the efficient extraction depend on the type of contaminant, degree of 30 contamination, type of well wood as lignocellulosic composite material to be produced. The lignocellulosic composites are bonded, if necessary, with synthetic adhesives such as urea-formaldehyde resins (UF),

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melamine-urea-formaldehyde resins (MUF), phenol-formaldehyde resins (PF), melamine-urea-phenol-formaldehyde resins (MUPF), melamine-formaldehyde resins (MF), isocyanate binders (PMDI) and others.

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Accordingly to the invention, therefore, there is provided a one-step method for extracting and decontaminating waste chemically treated wood such as creosote-, CCA-, PCP- treated etc., and simultaneously defibrating it to fibres suitable for the manufacture of lignocellulosic composite materials. The treatment is carried out in alkaline conditions at 40° to 100°C accompanied by the application of high shear forces on the wood in a low pressure environment.

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The method involves the treatment of waste chemically treated wood at from  $40^{\circ}\text{C}$  to  $100^{\circ}\text{C}$ . Most preferably the range is between  $60^{\circ}\text{C}$  to  $80^{\circ}\text{C}$ .

A typical operating pressure in the system would be from 1 to 2 atm.

The present method can be carried out in any high shear device at shearing intensities in the range of 250-25 300 kWh/ton of dry wood. The treatment according to the invention is thus conducted in a high shear-mixing device operated at low pressure close to the atmospheric (1 atm) under specific chemical, thermal and mechanical conditions. Use of a conventional twin-screw extruder device in accordance with a preferred embodiment of the invention provides the requisite high shear application.

The high shear forces to be applied depend on the wood material and the types of chemicals added to the substrate.

35 Moreover, dilute alkali like sodium hydroxide or sodium

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sulphite along with special emulsifiers like o,m,p, dodecyl sulfonic acid, or additives of chelatant, or sequestrants like ethylene diamine tetracetate are usually applied. In overall, the aforesaid reagents are used in the form of water solution or suspension in quantities between 0.01-5% based on dry wood.

Following the defibration, and for dry processes, the fibres produced can be washed, neutralised (if necessary), 10 blended with a synthetic resin and additives, and finally dried using conventional air dryers (e.g. flash dryers) in a continuous process. From then onwards, the dried fibres follow the conventional procedure as for the production of medium density fibreboards. Alternatively, and for the production of wet process fibreboards, the known conventional processes can be similarly applied, following the process in the high shear device.

The starting materials (wood chips) can be obtained by 20 mechanically disintegrating waste chemically treated wood, i.e. timbers, poles, posts, in conventional hammermills.

The invention is illustrated by the examples which follow, given without limitation:

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#### EXAMPLE 1

A CCA-treated post was disintegrated in chips by utilising a conventional hammermill. 10 kg of such chips 30 were introduced in a lab scale twin-screw extruder, operated at atmospheric pressure, extracted and defibrated using an alkaline system of 0.4% sodium hydroxide (on dry wood) and 0.2% ethylene diamine tetracetate (on dry wood) at 80°C. This alkaline 35 treatment was very efficient and the extraction of

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contaminated wood in the extruder removed 99.8% of copper and chromium and 99.9% of arsenic.

#### EXAMPLE 2

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A waste creosote-treated electricity pole of an approx. 25% degree of contamination (on the dry basis) was disintegrated in chips by utilising a conventional lab chipper. 10 kg of such chips were introduced in the 10 mentioned extruder, extracted, decontaminated and defibrated using an alkaline system of 0.4% sodium hydroxide (on dry wood) and 0.1% o,m,p dodecyl sulfonic acid (on dry wood) at 80°C. This alkaline extraction removed approx. 99% of all creosote compounds.

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#### EXAMPLE 3

The fibres produced from Example 2 were dried and used for the production of lab-scale MDF fibreboards of 16mm 20 thickness after mixing with a conventional UF resin. The resin level employed was 12%, the pressing temperature was 200°C, the pressing time was 15sec/mm and the press pressure was 35Kg/cm². Three replicate boards were produced and their properties were subsequently determined. The values of 25 board properties are presented in the Table below.

The formaldehyde (HCHO) emission was determined by using the Perforator method. As it can be seen from the results of this test, the decontaminated fibres generated from 30 waste creosote-treated wood gave MDF boards with quite high internal bond and bending strength properties. The quality of the boards produced in overall was very satisfactory.

Lab MDF boards	1	2	3
Internal bond (IB) strength, N/mm <sup>2</sup>	0.60	0.57	0.55
Modulus of rupture (MOR), N/mm <sup>2</sup>	20.3	21.0	19.7
24h swell, %	13.5	14.0	14.5
HCHO, mg/100g board	10.2	9.5	9.6

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#### CLAIMS:

1. A process for extracting and decontaminating waste chemically treated wood and simultaneously defibrating 5 to fibres suitable for the manufacture lignocellulosic composite materials, in which waste chemically treated exterior-use wood is subjected in particle form to a combined chemical-thermal-mechanical treatment in an aqueous alkaline system, in the presence of a chemical additive which is selected from 10 emulsifiers and decontamination dilute bases, disintegration agents, at 40° to 100°C under a highshear force at intensities of 250-300 kWh/ton dry wood, the system operating at a low pressure close to the 15 atmospheric.

2. A process according to claim 1, wherein the waste chemically treated wood comprises creosote-, chromated copper arsenate- and pentachlorophenol-treated wood.

- 3. A process according to any one of claims 1 and 2 in which the chemical-thermal-mechanical treatment is carried out in a twin-screw extruder.
- 25 4. A process according to any one of claims 1 to 3 in which waste chemically treated wood is mechanically disintegrated into chips before the chemical-thermal-mechanical treatment.
- 30 5. A process according to any one of claims 1 to 3, wherein the waste chemically treated wood is extracted, decontaminated and defibrated in the presence of 0.01-5% by weight sodium hydroxide.

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6. A process according to any one of claims 1 to 3, wherein the waste chemically treated wood is extracted, decontaminated and defibrated in the presence of 0.01-5% by weight sodium sulphite.

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7. A process according to any one of claims 1 to 3, wherein the waste chemically treated wood is extracted, decontaminated and defibrated in the presence of o,m,p dodecyl sulfonic acid as an emulsifier.

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8. A process according to any one of claims 1 to 3, wherein the waste chemically treated wood is extracted, decontaminated and defibrated in the presence of additives of chelatant.

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9. A process according to any one of claims 1 to 3, wherein the waste chemically treated wood is extracted, decontaminated and defibrated in the presence of ethylene diamine tetracetate as sequestrant.

## INTERNATIONAL SEARCH REPORT

Inter onal Application No PCT/GR 00/00020

A. CLASSI IPC 7	FICATION OF SUBJECT MATTER B27K3/00 A62D3/00 B27N1,	/00	
According to	o International Patent Classification (IPC) or to both national clas	ssification and IPC	
B. FIELDS	SEARCHED	_	
Minimum do IPC 7	ocumentation searched (classification system followed by classif B27K A62D B27L B27N	fication symbols)	
Documenta	tion searched other than minimum documentation to the extent t	hat such documents are included in the fields so	earched
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C. DOCUM	ENTS CONSIDERED TO BE RELEVANT		
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X Furt	ther documents are listed in the continuation of box C.	Patent family members are listed	l in annex.
"A" docum consi "E" earlier filing docum which citatic "O" docum other "P" docum later t	ent which may throw doubts on priority claim(s) or is cited to establish the publication date of another on or other special reason (as specified) nent referring to an oral disclosure, use, exhibition or means ent published prior to the international filing date but than the priority date claimed	"T" later document published after the inte or priority date and not in conflict with cited to understand the principle or the invention  "X" document of particular relevance; the cannot be considered novel or cannot involve an inventive step when the de  "Y" document of particular relevance; the cannot be considered to involve an indocument is combined with one or ments, such combination being obvious in the art.  "&" document member of the same patent	n the application but leavy underlying the claimed invention of the considered to occument is taken alone claimed invention occumed invention of the considered the core other such docupus to a person skilled
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Name and	mailing address of the ISA  European Patent Office, P.B. 5818 Patentlaan 2  NL – 2280 HV Rijswijk  Tel. (+31–70) 340–2040, Tx. 31 651 epo nl,	Authorized officer  Dalkafouki A	

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